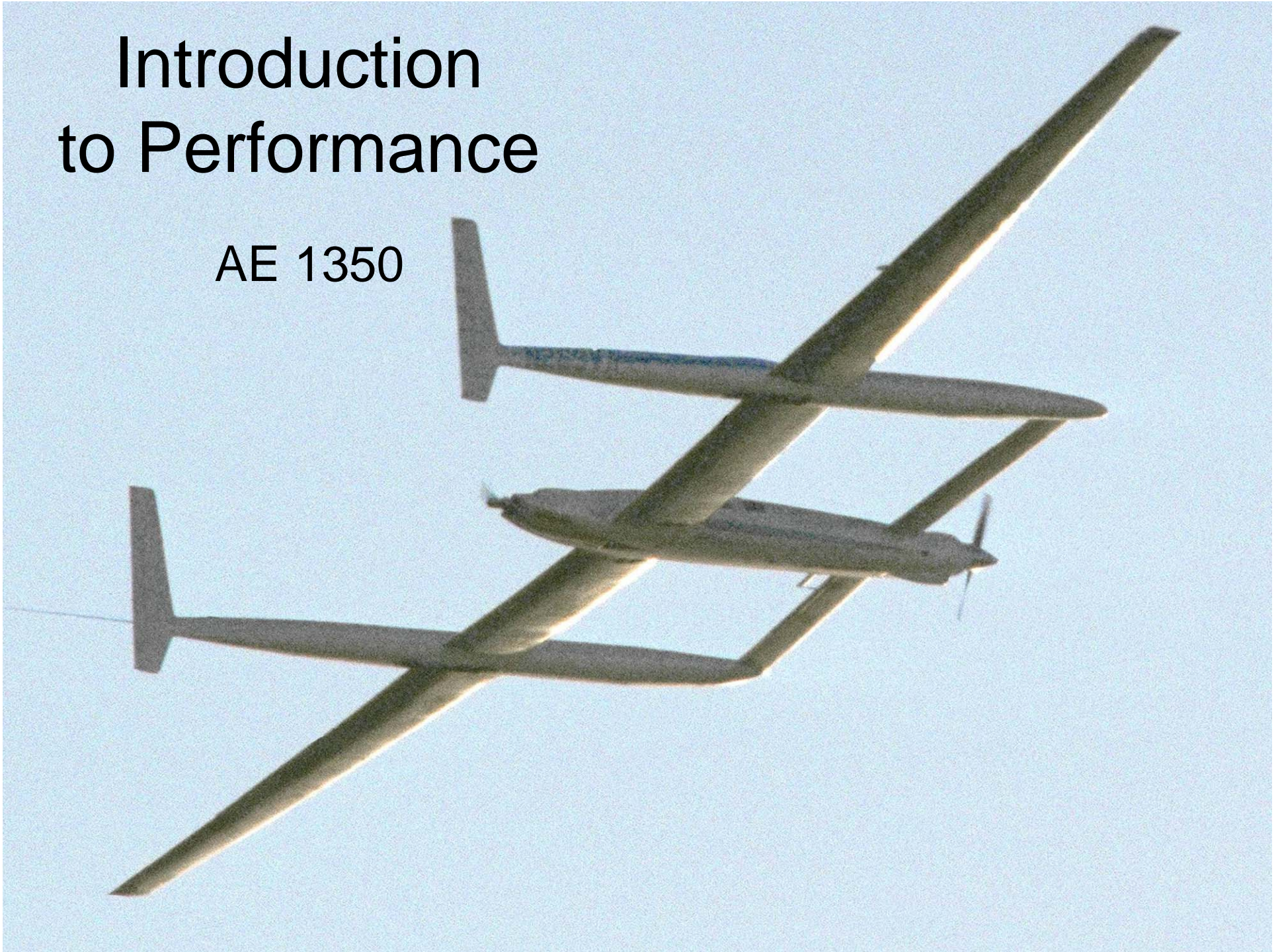


# Introduction to Performance

AE 1350



Performance: A measure of how well a device does its job

### *Airplane Performance Examples*

Speed -> how fast/slow can it go?

Rate of Climb -> how fast can it go up?

Ceiling -> how high can it go?

Range -> how far can it go?

Endurance -> for how long can it fly?

Takeoff/Landing -> how much runway does it need?

Turning -> what is the minimum turn radius?



## *Helicopter Performance Examples*

Hover Capability -> how much weight can it lift vertically?

Speed -> how fast can it go?

Rate of Climb -> how fast can it go up?

Ceiling -> how high can it go?

Range -> how far can it go?

Endurance -> for how long can it fly?



## *Launch Vehicle/Rocket Performance Examples*

Payload Mass to Low-Earth Orbit

Payload Mass to Geosynchronous Orbit

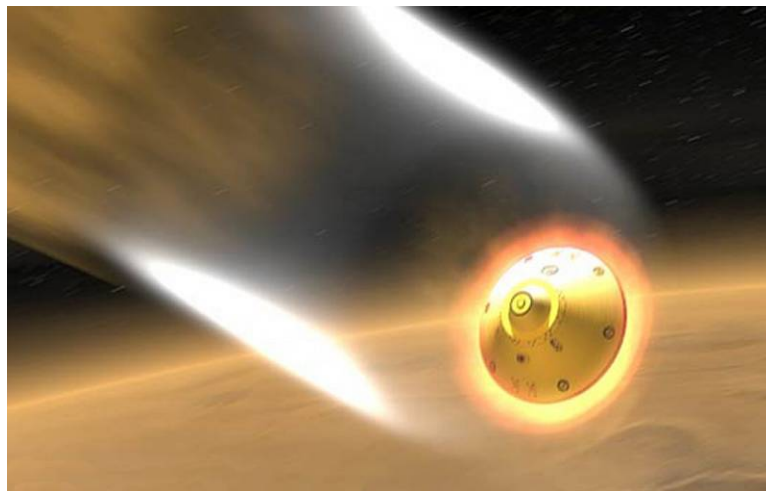
Change in Velocity  $\Delta V$



## *Entry, Descent, and Landing Vehicle Performance Examples*

Landed Mass

Landing Accuracy

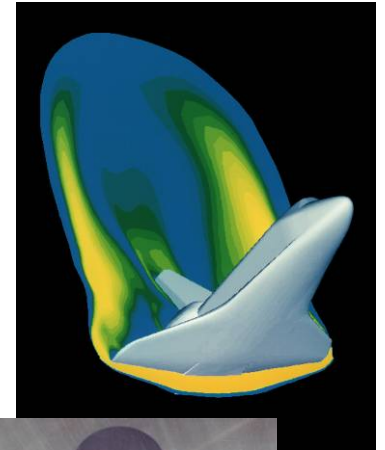


# How is Aerospace Vehicle Performance Calculated?

Aerospace vehicle performance is determined by using one or more of the following:

## Mathematical Modeling

- Computational Fluid Dynamics
- Classical aero/propulsive/mass analyses



## Ground Testing

- Wind tunnel testing
- Static engine testing

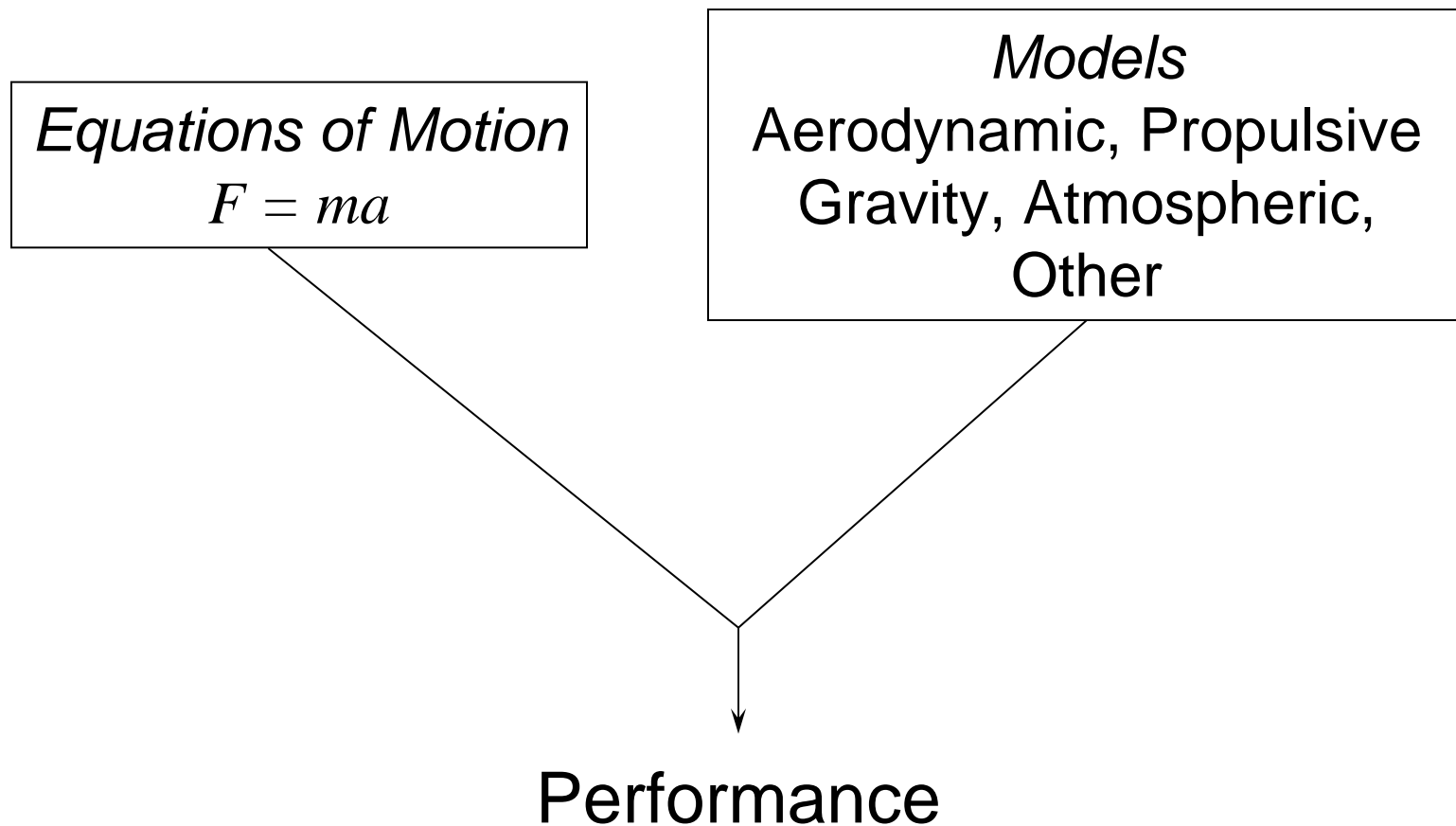


## Flight Testing



# Airplane Performance

## General Approach



# Airplane Performance

## Aerodynamic Models

The lift,  $L$ , and drag,  $D$ , of the airplane can be calculated from:

$$L = \frac{1}{2} \rho V^2 S C_L$$

$$D = \frac{1}{2} \rho V^2 S C_D$$

Where:

$\rho$  is the atmospheric density

$V$  is the airspeed

$S$  is the wing area

$C_L$  is the lift coefficient

$C_D$  is the drag coefficient

# Airplane Performance

## Aerodynamic Models - continued...

We will model the relationship between the lift and drag of an airplane through the drag polar:

$$C_D = C_{D0} + KC_L^2$$

Where we know the values of  $C_{D0}$  and  $K$  for our airplane.

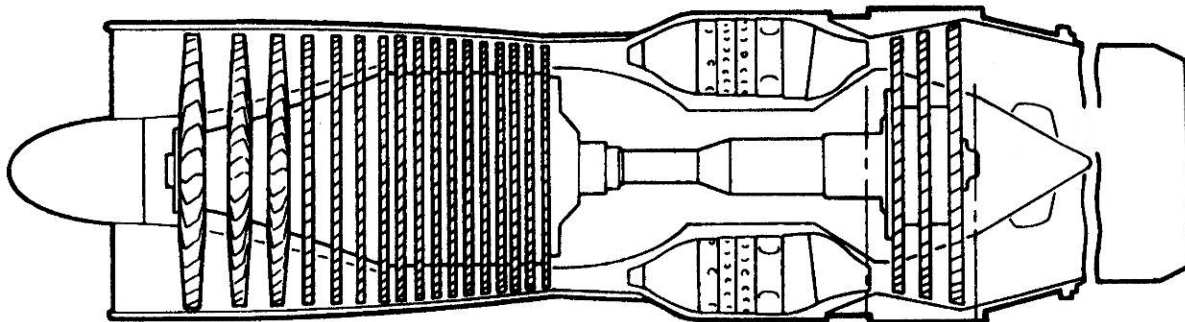
The lift coefficient,  $C_L$ , has a known maximum value:

$$C_{L,Max}$$

# Airplane Performance

## Propulsion Models

In this introduction to performance lecture we will assume all our airplanes are using turbojet engines (no bypass):



# Airplane Performance

## Propulsion Models - continued...

For a turbojet engine, maximum thrust,  $T_{Max}$ , does not change very much with airspeed,  $V$ , while flying at subsonic speeds

For a turbojet engine the maximum thrust,  $T_{Max}$ , changes with density as given by:

$$T_{Max} = T_{Max0} \left( \frac{\rho}{\rho_0} \right)$$

Where,

$\rho_0$  is the atmospheric density at sea level

$T_{Max0}$  is the maximum thrust at sea level

# Airplane Performance

## Propulsion Models - continued...

How do we quantify the fuel consumption of a turbojet engine? We usually do so by calculating the thrust specific fuel consumption,  $c_t$ :

$$\begin{aligned}c_t &= \text{thrust specific fuel consumption} \\ &= \frac{\text{(weight of fuel consumed for a given time increment)}}{\text{(thrust output)} \cdot \text{(time increment)}} \\ &= \frac{\dot{W}_{fuel}}{T}\end{aligned}$$

In this lecture we will treat  $c_t$  as a constant

At subsonic speeds  $c_t$  is constant;  
It does not vary much with velocity or altitude

# Steady Level Flight

By definition, lift is perpendicular to the wing and  $V$

By definition drag is parallel to  $V$

No acceleration (steady),  $V = \text{constant}$

Wings level

Horizontal flight (no climb/descent)

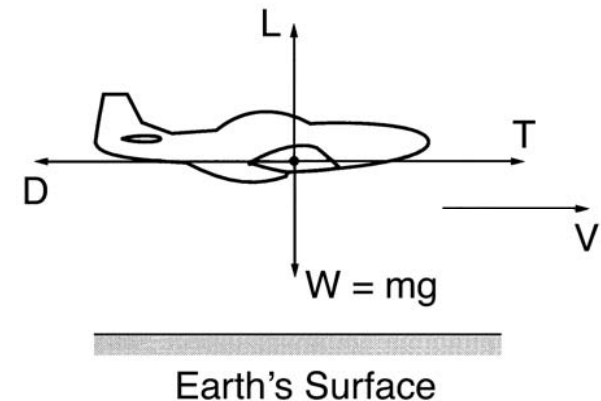
Usually the magnitude of  $L$  and  $W$  are greater than  $D$  and  $T$

Summing forces parallel to the flight direction:

$$T - D = 0 \quad \text{or equivalently} \quad T = D$$

Summing forces perpendicular to the flight direction:

$$L - W = 0 \quad \text{or equivalently} \quad L = W$$



# Stall Speed

Let us determine how slow we can fly in steady level flight. In other words, we want to determine the stall speed,  $V_{stall}$

$$L = \frac{1}{2} \rho V^2 S C_L = W$$

$$V = \sqrt{\frac{2W}{\rho S C_L}}$$

How do we minimize  $V$  for a given airplane?

By flying at  $C_{L,Max}$ !

$$V_{stall} = \sqrt{\frac{2W}{\rho S C_{L,Max}}}$$

# Stall Speed

$$V_{stall} = \sqrt{\frac{2W}{\rho S C_{L,Max}}}$$

How does the various parameters in this equation:

$$W, \rho, S, C_{L,Max}$$

affect  $V_{stall}$ ?

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Numerical Example: Motorglider

$$m = 300 \text{ kg}$$

$$W = mg = 2,943 \text{ N}$$

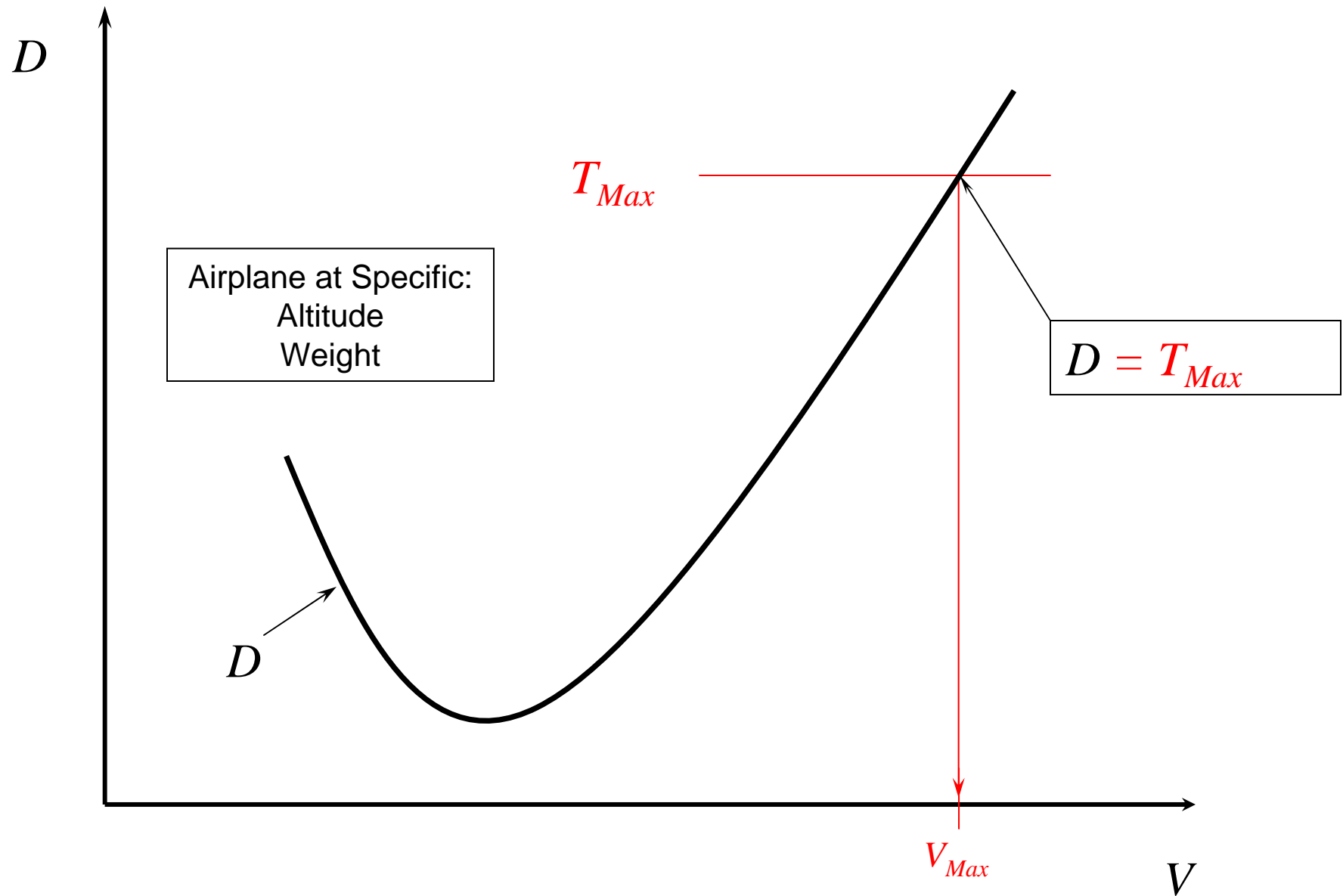
$$\rho = 1.225 \text{ kg/m}^3 \text{ (i.e., sea level)}$$

$$S = 12.5 \text{ m}^2$$

$$C_{L,Max} = 1.5$$

$$V_{stall} = 16 \text{ m/s}$$

# Maximum Speed



# Maximum Speed

To determine the maximum speed of a turbojet airplane we start with the equation of motion:

$$T = D$$

But we agreed to model the thrust as:

$$T = T_{Max} = T_{Max0} \left( \frac{\rho}{\rho_0} \right)$$

and determine drag from:

$$D = \frac{1}{2} \rho V^2 S C_D$$

Substituting these equations into the first one gives us:

$$T_{Max0} \left( \frac{\rho}{\rho_0} \right) = \frac{1}{2} \rho V^2 S C_D$$

# Maximum Speed

We also agreed to a drag polar model for  $C_D$  of the form:

$$C_D = C_{D0} + KC_L^2$$

This equation has  $C_L$  in it... Let's see if we can get rid of it by writing  $C_L$  in terms of  $V$ . From our other equation of motion we already know that:

$$L = \frac{1}{2} \rho V^2 S C_L = W$$

Solving this equation for  $C_L$  gives us:

$$C_L = \frac{2W}{\rho V^2 S}$$

Substituting this equation for  $C_L$  into our polar model yields:

# Maximum Speed

$$C_D = C_{D0} + K \frac{4W^2}{(\rho V^2 S)^2}$$

Which we can then plug in onto our equation relating thrust and drag:

$$T_{Max0} \left( \frac{\rho}{\rho_0} \right) = \frac{1}{2} \rho V^2 S C_D$$

to get, after some rearranging:

$$T_{Max0} \left( \frac{\rho}{\rho_0} \right) = \frac{1}{2} \rho V^2 S C_{D.0} + \frac{2KW^2}{\rho V^2 S}$$

Multiplying both sides of this equation by  $V^2$  gives us:

# Maximum Speed

Which, after some rearranging gives us:

$$\left[ \frac{1}{2} \rho S C_{D0} \right] V^4 - \left[ T_{Max0} \left( \frac{\rho}{\rho_0} \right) \right] V^2 + \frac{2KW^2}{\rho S} = 0$$

Notice that this is simply a quadratic equation in  $V^2$  of the form:

$$a(V^2)^2 + bV^2 + c = 0$$

Where,

$$a = \left[ \frac{1}{2} \rho S C_{D0} \right] \quad b = \left[ -T_{Max0} \left( \frac{\rho}{\rho_0} \right) \right] \quad c = \left[ \frac{2KW^2}{\rho S} \right]$$

# Maximum Speed

This quadratic equation has a solution of the form:

$$V^2 = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

I leave it up to you to complete the gory algebra to show that:

$$V = \sqrt{\frac{T_{Max0} \left( \frac{\rho}{\rho_0} \right) \pm \sqrt{T_{Max0}^2 \left( \frac{\rho}{\rho_0} \right)^2 - 4C_{D0}KW^2}}{\rho SC_{D0}}}$$

Finally, we are interested in the maximum speed,  $V_{Max}$ , so we pick the positive root in the above equation to yield...

# Maximum Speed

$$V_{Max} = \sqrt{\frac{T_{Max0} \left( \frac{\rho}{\rho_0} \right) + \sqrt{T_{Max0}^2 \left( \frac{\rho}{\rho_0} \right)^2 - 4C_{D0}KW^2}}{\rho SC_{D0}}}$$

---

Numerical Example: Motorglider Powered by a Turbojet (Wow!)

$$m = 300 \text{ kg}$$

$$W = mg = 2,943 \text{ N}$$

$$\rho = 0.6601 \text{ kg/m}^3 \text{ (i.e., 6,000 m altitude)}$$

$$\rho_0 = 1.225 \text{ kg/m}^3 \text{ (i.e., sea level)}$$

$$S = 12.5 \text{ m}^2$$

$$C_{D0} = 0.015$$

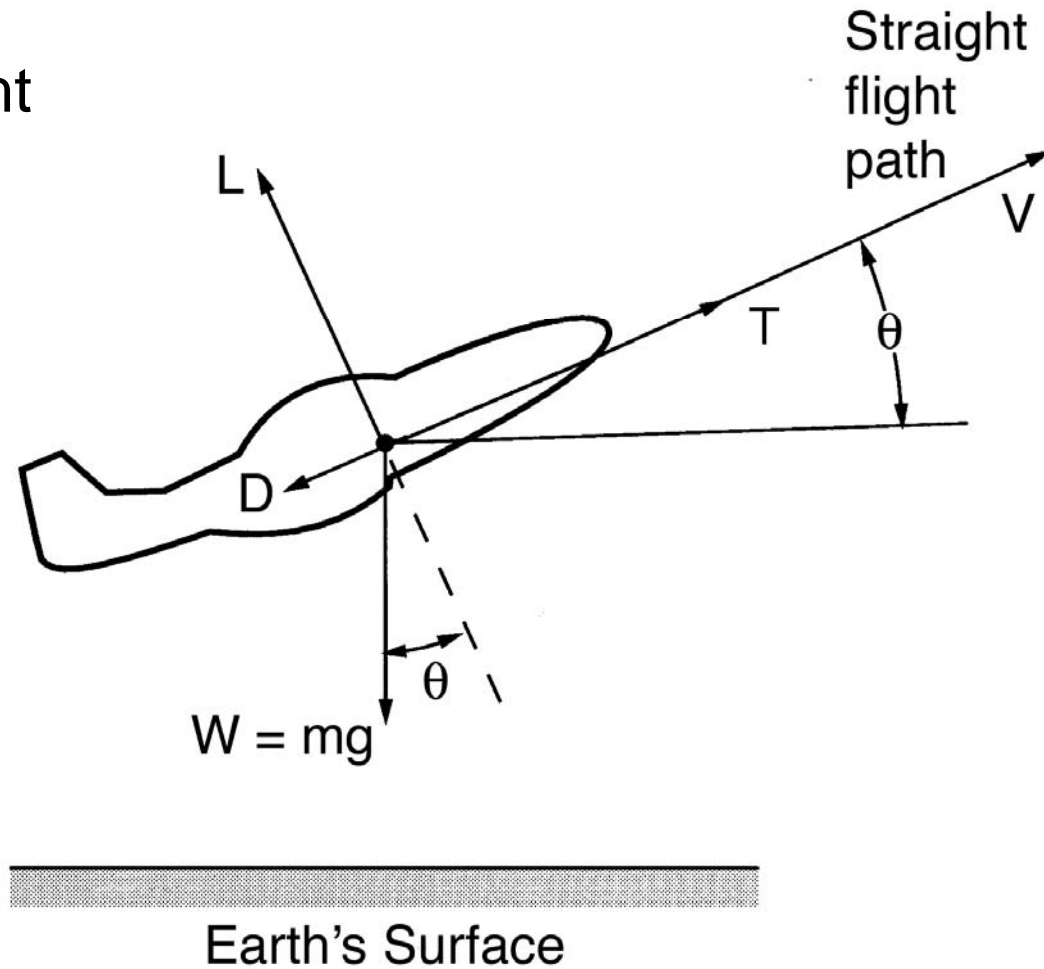
$$K = 0.020$$

$$T_{Max0} = 500 \text{ N}$$

$$V_{Max} = 64.7 \text{ m/s}$$

# Rate of Climb

## Steady Climbing Flight



$\theta$  - flight path angle with respect to horizon (positive as shown)

Note: arrows not to scale!

# Rate of Climb

No acceleration (steady)

Wings level

Climbing flight at an angle  $\theta$   
to Earth's surface

Thrust parallel to velocity

Summing forces parallel to the flight  
direction:

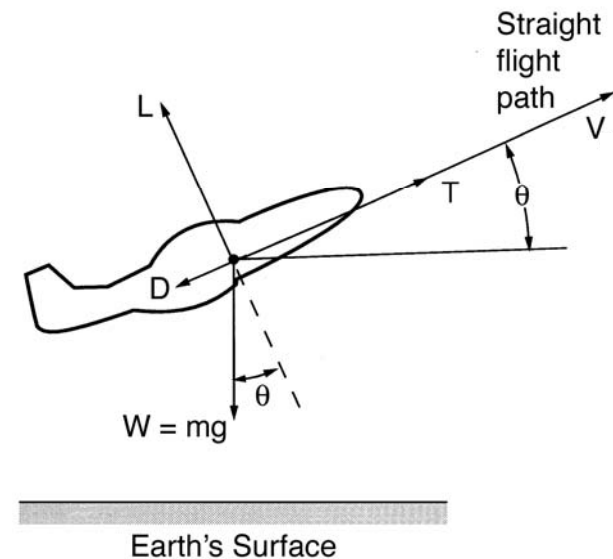
$$T - D - W \sin\theta = 0$$

Summing forces perpendicular to the flight direction:

$$L - W \cos\theta = 0$$

Rate of Climb = ROC =  $V \sin\theta$

Note that the same equations apply to steady descending flight!



# Rate of Climb

Starting with the sum of forces parallel to the flight direction:

$$T - D - W \sin\theta = 0$$

Multiply by  $V$  and re-arrange:

$$\frac{TV - DV}{W} = V \sin\theta = \text{ROC}$$

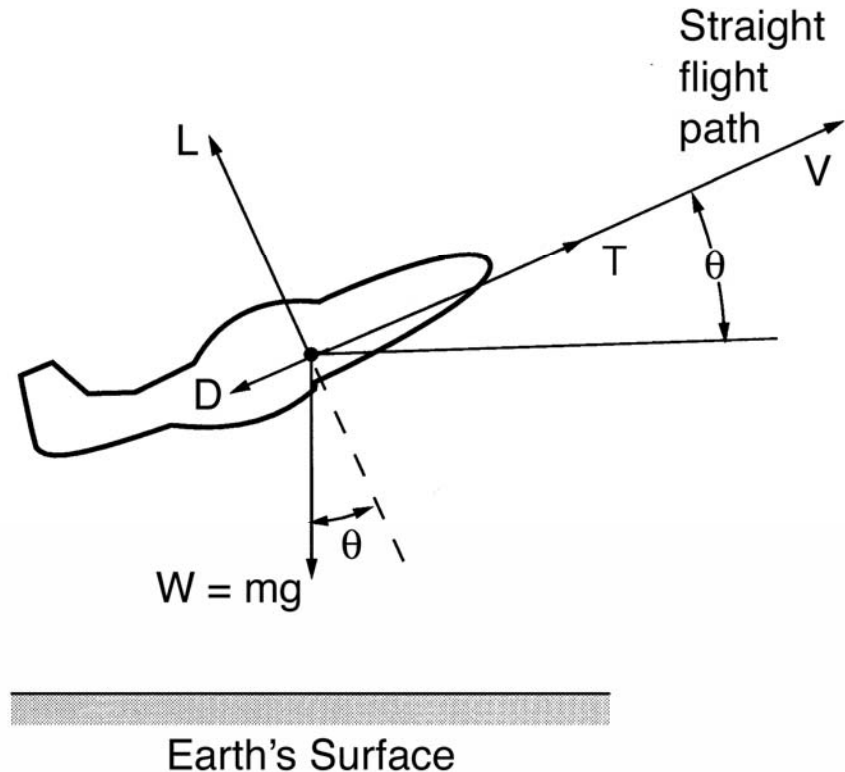
Note that:

$$T V = P_A = \text{Power Available}$$

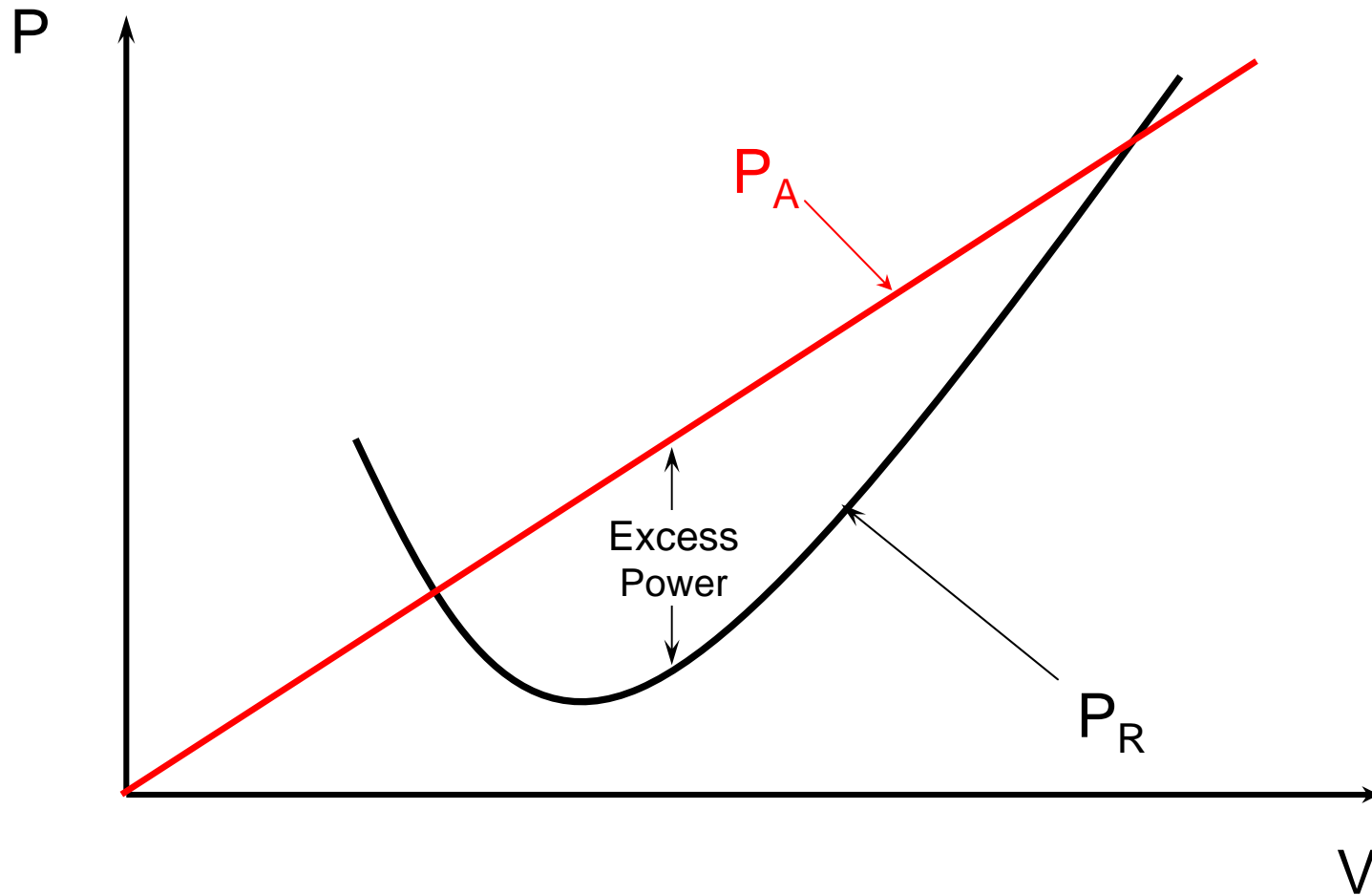
$$D V = P_R = \text{Power Required}$$

Thus,

$$\text{ROC} = \frac{\text{Power Available} - \text{Power Required}}{W} = \frac{\text{Excess Power}}{W}$$



# Rate of Climb



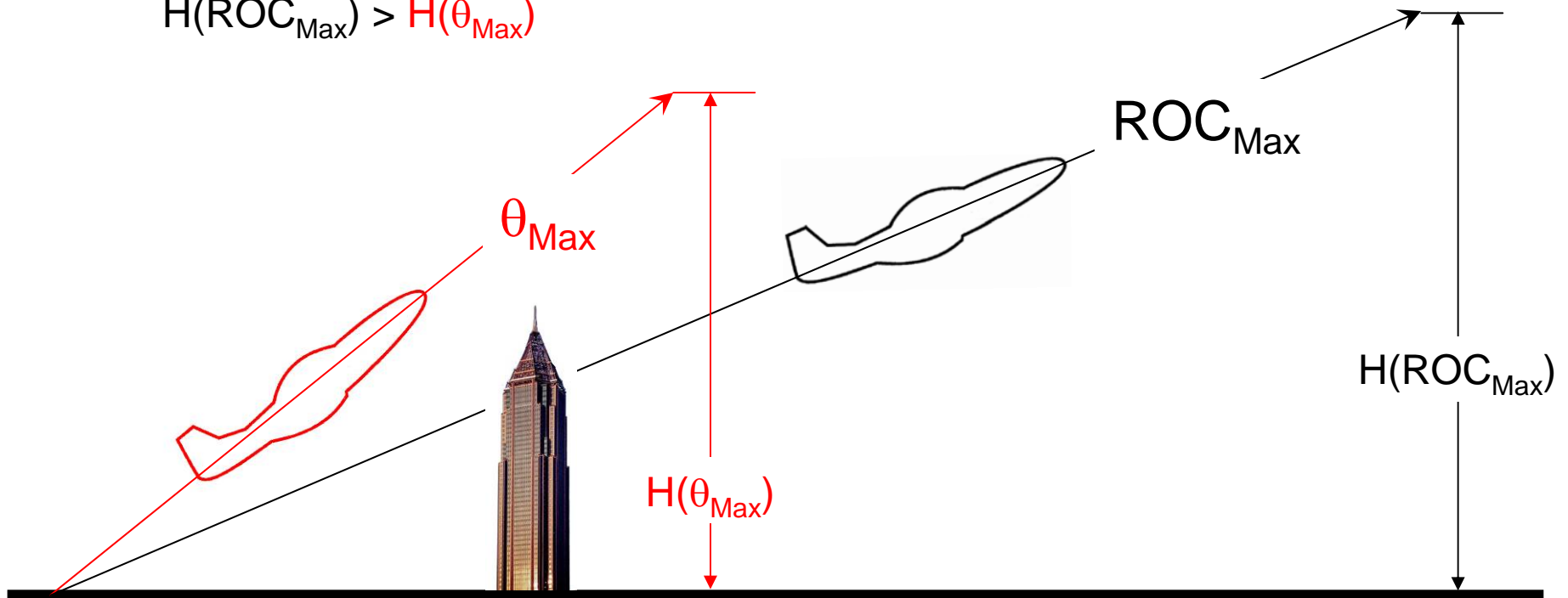
$$\text{ROC} = \frac{TV - DV}{W} = \frac{P_A - P_R}{W} = \frac{\text{Power Available} - \text{Power Required}}{W} = \frac{\text{Excess Power}}{W}$$

# Rate of Climb

Here we have discussed the rate of climb, ROC. A related problem is the angle of climb,  $\theta$ . Note that the maximum rate of climb,  $ROC_{Max}$  does not yield the maximum angle of climb,  $\theta_{Max}$ . Pilots beware!!!

After same time interval:

$$H(ROC_{Max}) > H(\theta_{Max})$$



# Range

Range - How far can we fly?

In this discussion we will try develop integral equations to calculate the range of an airplane during its cruise leg.

Range will be significantly affected by weight, so let us start by defining some weight quantities. Let:

$W_0$  - Weight of the airplane at the start of cruise leg

$W_f$  - weight of fuel at a specific point in time; varies throughout the cruise leg

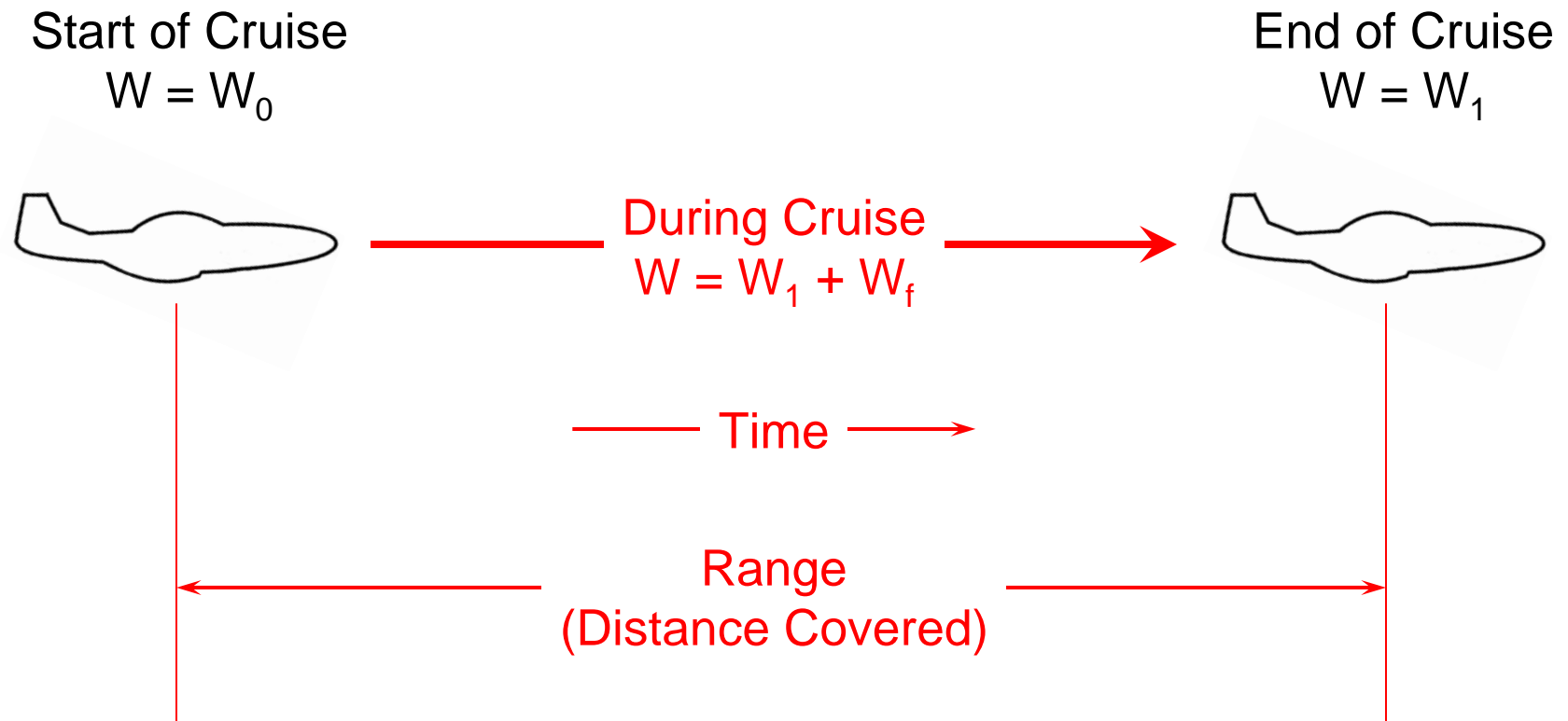
$W_1$  - weight of the airplane at the end of the cruise leg

$W$  - weight of the airplane at a specific point in time; varies throughout the cruise leg

At any point during the cruise leg, then:

$$W = W_1 + W_f$$

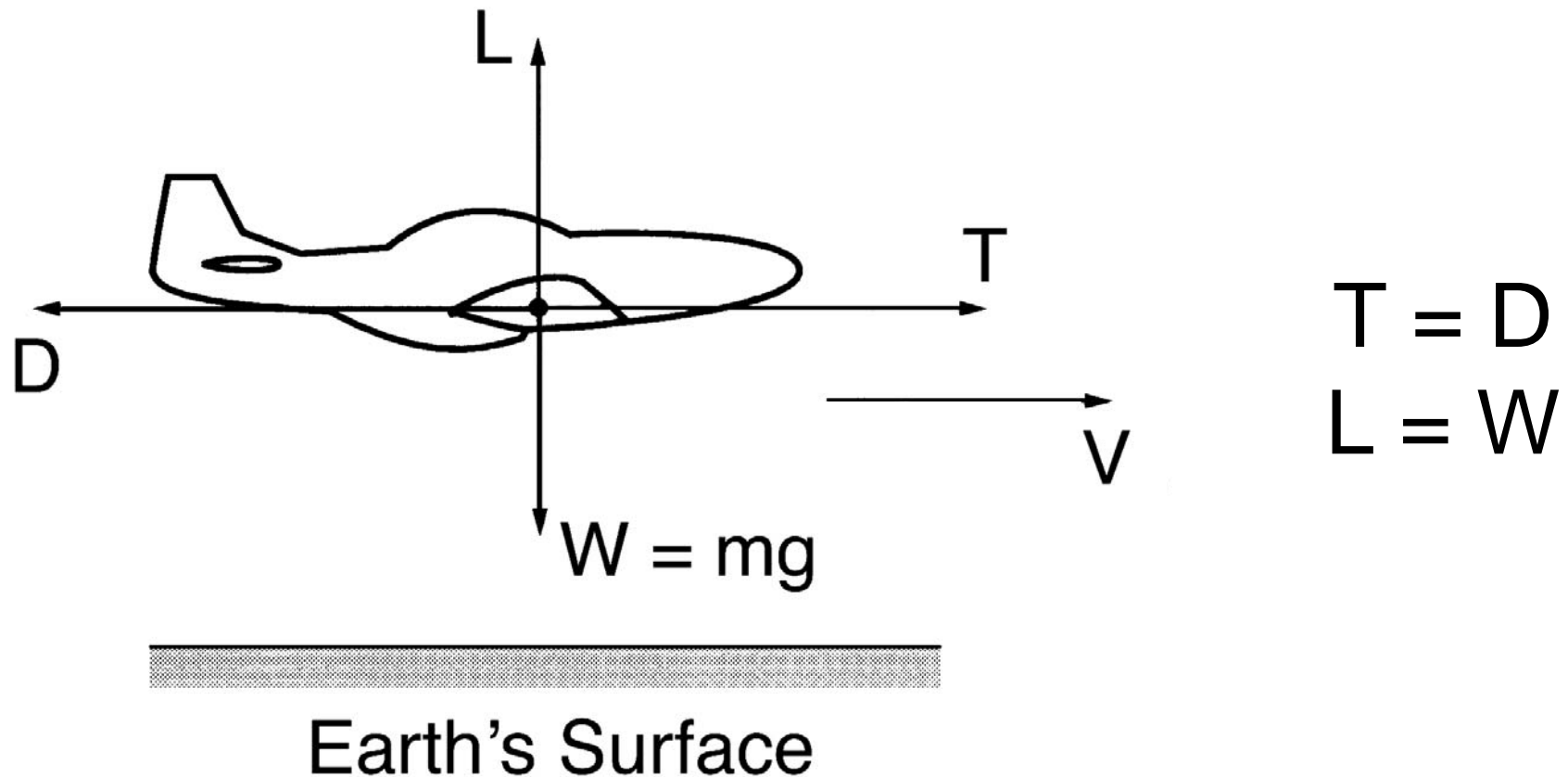
# Range



*Note: No assumption is being made about the flight altitude at this time - altitude during cruise may or may not be constant!*

# Range

Let us assume we are in level steady flight, and that our thrust vector is aligned with the airspeed:



# Range

After a certain amount of calculus and manipulation we can write the following integral equation for the range,  $R$ , of a turbojet airplane:

$$R = \int_{W_1}^{W_0} \frac{V}{c_t} \frac{L}{D} \frac{dW}{W} = \int_{W_1}^{W_0} \frac{1}{c_t} \sqrt{\frac{2}{\rho S}} \frac{C_L^{1/2}}{C_D} \frac{dW}{\sqrt{W}}$$

Very few assumptions were made to derive this equation:

- Flight in no-wind conditions
- Steady level flight  
 $L = W$   
 $T = D$
- Thrust aligned with  $V$

# Range

We can make some further assumptions and that will simplify the integral and allow us to evaluate it explicitly:

- The thrust specific fuel consumption,  $c_t$  is constant
- We are flying at a constant altitude, thus  $\rho$  is constant
- The wing area,  $S$ , is constant (we hope so!)
- We are flying at a constant value of  $(C_L^{1/2}/C_D)$

These assumptions allow us to move various quantities in front of the integral:

# Range

$$R = \frac{1}{c_t} \sqrt{\frac{2}{\rho S}} \frac{C_L^{1/2}}{C_D} \int_{W_1}^{W_0} \frac{dW}{\sqrt{W}}$$

Now we can evaluate this integral explicitly:

$$R = \frac{2}{c_t} \sqrt{\frac{2}{\rho S}} \frac{C_L^{1/2}}{C_D} (W_0^{1/2} - W_1^{1/2})$$

This is one version of the range equation for a turbojet airplane.

# Range

$$R = \frac{2}{c_t} \sqrt{\frac{2}{\rho S}} \frac{C_L^{1/2}}{C_D} (W_0^{1/2} - W_1^{1/2})$$

What is this equation telling us about obtaining maximum range for a turbojet airplane?

- For maximum range, fly at the value of  $C_L$  where  $(C_L^{1/2}/C_D)$  is maximum.
- Fly at high altitude so that  $\rho$  is small (within limits...).
- Use an efficient engine with a low value of  $c_t$ .
- Carry lots of fuel.

# Range

A similar equation can be derived for an airplane powered by a reciprocating engine/propeller combination:

$$R = \frac{\eta_{pr}}{c} \frac{C_L}{C_D} \ln \frac{W_0}{W_1}$$

Where,

$\eta_{pr}$  is the propeller efficiency

$c$  is the power specific fuel consumption

This is one of the best known equations in aeronautics. It is known as the Breguet Range Equation.

What is this equation telling us about obtaining maximum range for a reciprocating engine/propeller airplane?